A Novel Hybrid Approach for Optimal Reactive Power Dispatch under Unbalanced Conditions

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Abstract: Recently, the Optimal Reactive Power Dispatch (ORPD) is gaining a considerable attention in the power systems, as they decide the security as well as economy of a power system. The major target behind this works is to upgrade the power system efficiency by means of optimally allocating the real power, so that the power loss should be minimized, and voltage profiles should be enhanced. With this intention, here an optimization algorithm referred as “Trial based Update on Whale and Particle swarm Algorithm (TU-WPA)” is implied, which is an amalgamation of two algorithms called, “Particle Swarm Optimization (PSO) and Whale Optimization Algorithm (WOA)”. The TU-WPA model fine tunes the key parameters like “load reactance; voltage and transformer tap settings”. Finally, the performance of the TU-WPA is compared over the existing works under “IEEE 14 and the IEEE 39 bus systems”. On observing the best performance of the adopted scheme, a higher value (0.35327) is recorded, while the compared models attain comparatively lower values, i.e. GA= 0.26496, FF= 0.27496, PSO= 0.256, ABC= 0.3296, WOA= 0.20333, DA= 0.29432 and CS= 0.30496.

Keywords: Optimal Reactive Power Dispatch; Active Power Loss Minimization; Voltage Profile Improvement; Inequality And Equality Constraints; TU-WPA

Nomenclature

Abbreviations	Descriptions
AP & RP	Active And Reactive Power
AP loss	Active Power Loss
ADMM	Alternating Direction Method Of Multipliers
ABC	Artificial Bee Colony
APL	Active Power Regulation
CS	Cuckoo Search
DERs	Distributed Energy Resources
DE	Differential Evolution
EFFA	Enhanced Firefly Algorithm
FF	Firefly Algorithm
GA	Genetic Algorithm
HMP SO	Hybrid Multi-Swarm Particle Swarm Optimisation
IPM	Interior Point Method
LP	Linear Programming
M-OOP	Multi-Objective Optimisation Problem
MORPD	Multi-Objective Optimal Reactive Power Dispatch
MODE	Multi-Objective Differential Evolution
OOAR-PDP	Objective Optimal Active And Reactive Power Dispatch Problems
ORPF	Optimal Reactive Power Flow
ORPD	Optimal Reactive Power Dispatch
OPF	Optimal Power Flow
PSO	Particle Swarm Optimization
QP	Quadratic Programming
QODE	Quasi-Oppositional Differential Evolution
QOBL	Quasi-Oppositional Based Learning
RPD	Reactive Power Dispatch

TC	Transfer Conductance
TU-WPA	Trial Based Update On Whale And Particle Swarm Algorithm
TLs	Transmission Line
VS	Voltage Stability
VD	Voltage Deviation
WOA	Whale Optimization Algorithm

1. Introduction

The Power firm of a country shapes the fundamental national foundation of that particular country's economy as it is the entrepreneur and innovatively escalated industry. In mid 80's the interest for power was low and thus little power stations were accessible in the area [6] [7]. The current day power framework is huge with numerous producing stations, as it has more popularity for farming, business and local shoppers. In these power advancements, the significant issues are the power framework strength [8] [22] [23]. The fundamental factor causing voltage unsteadiness is the failure of the power framework in fulfilling the responsive power need at intensely focused on frameworks, and this keeps it from keeping up the ideal voltages [9] [10] [11]. The receptive power/voltage control limits, responsive power repaying gadgets just as the heap qualities are the elements contributing the voltage breakdown. It is basic to streamline the receptive power dispatch so as to keep up the voltage dependability, power framework misfortunes and to control the activities of the influence framework [12] [13][33].

The APL and the RPD are the two significant imperatives for the practical activity of a power framework [14] [15]. The expense of creation of RP is regularly low, yet it presents colossal downsides on the active power transmission misfortune just as active power production. In the TLs, the active power stream as far as the transmission just as dispersion voltage should be controlled with responsive power [20] [21]. The OPF is proficient in deciding the ideal settings for not many of the factors concerning the power framework control so as to decide the target capacities in regards to the framework boundaries [16][34] [35]. the main sub problems of OPF is optimal reactive power dispatch (ORPD) problem which includes generator output voltages, compensators, tap ratios of transformers, and outputs of shunt reactive sources. This sub problem is used to minimize interested objective functions such as transmission losses while satisfying a given set of operating and physical limitations. The whole ORPD problem is considered as a non-linear multi-modal optimization problem with a combination of discrete and continuous variables. In addition, the sub-issue of OPF is the ORPF and its significant target is to reduce the "AP loss and maximization of voltage profile and stability real power loss" with the guide of influence framework control factors changes like "AP loss and maximization of voltage profile and stability". In the customary methodologies, a few exemplary improvement procedures like LP, QP and IPM were utilized to supersede the issues identified with advancement of the receptive power dispatch [17] [18] [19]. In any case, they flopped in accomplishing the worldwide minima and experienced unpredictability. Therefore, it is basic to have an ideal method, to defeat these difficulties. Moreover, the deployment of the optimization algorithm [25] [26] [36] will be a solution for most of the optimizations problems. The major contribution of this paper is as follows:

- Enhances the efficiency of power system by optimizing the real power allocation parameters such as load reactance; voltage and transformer tap settings using a new metaheuristic algorithm.
- Introduces Trial based Update on Whale and Particle swarm Algorithm, which is an amalgamation of two algorithms namely PSO and WOA.

The leftover sections of this paper are organized as: Section II reviews the recent works undergone relating the current research work. Section III tells about the optimal RP dispatch under unbalanced conditions: Objective function. Section IV depicts the TU-WPA algorithm for optical RP dispatch: Solution encoding. The resultants acquired with the TU-WPA are discussed in Section V. Finally, a strong conclusion is provided to the current research work in Section VII.

2. Literature Review

2.1 Related Works

In 2015, Srivastava and Singh [1] have developed a HMPSO algorithm for RP dispatch issues solving. The HMPSO was the amalgamation of the DE and the PSO. "The RPD problem is formulated as non-linear, constrained M-OOP with equality and inequality constraints for minimisation of power losses and improvement of voltage profile simultaneously". The proposed model was tested on "standard IEEE 30-bus and practical 75-bus Indian systems".

In 2015, Liang et al. [2] have proposed EFA with the intention of solving the power dispatch problems in terms of "AP & RP" in the wind generation unit. the authors have considered the RP as well as the active power's optimal dispatches at the same time. the losses in the TLs as well as the VD in the load buses were reduced by the RP dispatch, which takes into consideration the parameters like "load tap changer positions of transformers, the RP injection of capacitors, and the voltages of slack bus and PV buses". They have utilized the "IEEE 30-bus system" in order to test the presented work in terms of OAR-PDP.

In 2016, Basu [3] has suggested MODE for MORPD. this was achieved by means of lessening the "active power transmission loss and VD and maximizing VS". All these were accomplished by varying control variables of the power system like the "terminal voltages, transformer taps and RP output of shunt VAR compensators". the presented work was tested for the achievement of the objective by means of implementing it on "IEEE 30-bus, 57-bus and 118-bus systems".

In 2015, Robbins and Garcia [4] have proposed a novel approach in DERs for regulating the voltage of the bus. They have formulated an OPF problem for radial power systems, by means of introducing a branch power flow modeling approach. in OPF, certain non-linear terms were leveraged and hence a convex QP was formed. In addition, they have developed a distributed algorithm based on the ADMM to solve the issues related to QP.

In 2014, Zhou et al. [5] have proffered quasi-oppositional differential evolution approach in a power system in order to solve the issues related to the RP dispatch problem. This QODE have utilized the QOBL in order to initialize the population. Further, with the proposed model, the control variables settings were found in terms of "generator terminal voltages, transformer tap settings and RP output of shunt VAR compensators". Thus, the presented work had gained the "minimum AP loss, improved voltage profile and enhanced VS". The presented work was tested on "IEEE 30-bus, 57-bus and 118-bus test systems".

In 2020, Ettappan et al. [33] have proposed the ORPD for real power loss minimization, voltage deviation minimization and voltage stability enhancement using ABC Algorithm. The ABC algorithm was used to find the setting of control variables such as generator voltage magnitude, tap position of tap changing transformer and reactive power output of the compensation devices. The proposed algorithm was tested on IEEE 30 and 57 bus systems, Simulation results shown that the proposed approach converges to better solutions and much faster than the earlier reported approaches in the literature.

3. Proposed ORPD Model

3.1 ORPD Model Under Unbalanced Condition

Under the unbalanced condition, the achievement of ORPD is highly challenging. Thus, this research work goes towards the objective of AP loss minimization as well as stability and voltage profile improvement in the unbalanced condition of the network. The dependent variables in the vector form are expressed in Eq. (1).

$$Z = [Po_{G1}, Vo_{1-1}, \dots, Vo_{1-NPQ}, Q_{G-1}, \dots, Q_{G-NG}] \quad (1)$$

Here, the voltage bus PQ ($i=1,2,\dots,NPQ$) is denoted as Vo_{ii} and the slack bus power is indicated using the notation Po_{G1} . The real power from the generator ($i=1,2,\dots,NG$) is denoted as Q_{Gi} . Here, the count of buses in the generator is denoted as NG . In addition, the available count of the PQ bus is symbolized as NPQ . The control variable vector is given by Eq. (2). In the voltage controlled bus, the terminal voltage is represented as Vo_{Gi} . Then, the overall number of shunt VAR compensator's is NC , and NT is the count of quantity of the tap clanging transformer's.

$$U = [Vo_{G-1}, \dots, Vo_{G-NG}, Q_{C-1}, \dots, Q_{C-NC}, t_1, \dots, t_{NT}] \quad (2)$$

Active Power Load Minimization: The equality as well as the inequality factors is generated by these selected parameters. The objective function of the current research work is manifested in Eq. (3).

$$Obj = \alpha F_a + (1 - \alpha) F_b \quad (3)$$

Here, F_a indicates the AP loss and F_b signifies the VD. The mathematical formula for AP loss minimization is mathematically expressed in Eq. (4).

$$F_a = Po_1 = \sum_{k=1}^N g_k [Vo_m^2 + Vo_n^2 - 2Vo_m Vo_n \cos(\delta_m - \delta_n)] \quad (4)$$

The AP loss of the system is denoted as Po_l . The count of TLss is depicted as N . Then, among the buses m^{th} and n^{th} , the k^{th} branch conductance is denoted as g_k . For the buses, m^{th} and n^{th} , the voltage phase angles are δ_m and δ_n , correspondingly.

VD: The voltage magnitude (V_i) reduction at varied loads of a bus system, from a predetermined reference value (V^{ref}) is utilized with the aim of enhancing the voltage profile. The improvement in voltage profile is mathematically exhibited in Eq. (5).

$$F_b = Vo_D = \sum_{i=1}^{LB} Po_f \psi(Vo^{\min} - Vo_m) + Po_f \psi(Vo_m - Vo^{\max}) \quad (5)$$

The step function $\psi(z)$ is expressed in Eq. (6)

$$\psi(x) = \begin{cases} 1; & \text{if } z \geq 0 \\ 0; & \text{otherwise} \end{cases} \quad (6)$$

The count of load buses LB in Eq. (7) can be given as

$$|Vo_m|^2 = |Vo_i|^2 - 2(\tilde{r}_{im} Po_{im} + \tilde{z}_{im} Q_{im}) + c_{im}(\cdot, Q) \quad (7)$$

The susceptance x of the line is mathematically shown in Eq. (8)

$$\tilde{r}_{im} = \text{Re}\{aa^H\} \otimes r_{im} + \text{Im}\{aa^H\} \otimes x_{im} \quad (8)$$

The resistance r of the line is shown in Eq. (9)

$$\tilde{x}_{im} = \text{Re}\{aa^H\} \otimes x_{im} - \text{Im}\{aa^H\} \otimes r_{im} \quad (9)$$

$$a = \begin{bmatrix} 1 & e^{-j2\pi/3} & e^{j2\pi/3} \end{bmatrix} \quad (10)$$

$$c_{im} = [z_{im}[S_{im}^*/Vo_i^*]] \otimes [z_{im}[S_{im_0}/Vo_i]] \quad (11)$$

$$z_{im} = r + jx \quad (12)$$

$$S_{im} = [Po_{im} + jQ_{im}] \otimes [\tilde{z}_{im}(Po_{im} - jQ_{im})] \quad (13)$$

$$\tilde{z}_{im} = z_{im} \otimes (a_i a_i^H) \quad (14)$$

“It is the necessity of an every buses in the power system to withstand the voltage that is below the normal operating conditions and these buses need to adapt themselves to the disturbance like change in load and system configuration. At present most of the major networks deteriorate due to the instability in voltage”. The VS is achieved by means of lessening the VS indicator. At every bus, the L -index value (L_n) specified the voltage condition that is distorted of that specific bus. Mathematically, the L_n of n^{th} bus is denoted as per Eq. (15), where $n = 1, 2, \dots, NPQ$. In addition here the PV bus count is represented as NPV. The sub-matrices of YBUS is denoted as Y_b and Y_a . Then, the constraints of PQ and PV bus are separated for YBUS and is expressed mathematically in Eq. (17).

$$L_n = \left| 1 - \sum_{m=1}^{NPV} F_{nm} \frac{Vo_m}{Vo_n} \right| \quad (15)$$

$$F_{nm} = [Y_a]^{-1} [Y_b] \quad (16)$$

$$\begin{bmatrix} I_{PQ} \\ I_{PV} \end{bmatrix} = \begin{bmatrix} Y_a & Y_b \\ Y_c & Y_d \end{bmatrix} \begin{bmatrix} V_{PQ} \\ V_{PV} \end{bmatrix} \quad (17)$$

Then, for the entire PQ buses, the L -Index value is expressed. Here, the value of L_n is fixed as 0 or 1 on the basis of the n^{th} bus VD as well as no load stipulations. Therefore, the objective function could be given by Eq. (18), where $L_n = 1, 2, \dots, NPQ$.

$$F_c = \max(L_n) \quad (18)$$

3.2 Inequality and Equality Constraints

“The inequality constraints are-non binding constraints and there is no necessity for the real power output to stay within its maximum limit”. The power system is controlled by the equality factors, which encloses the load flow formulations. Mathematically, these load flow formulations are expressed in Eq. (19) and (20), respectively, where $m = 1, 2, \dots, NB$. The count of buses is represented as NB. the generation

of AP & RPs in m^{th} bus is denoted as P_{Gm} and Q_{Gm} , respectively. With respect to demand, the AP & RPs of m^{th} bus is specified as P_{Dm} and Q_{Dm} , respectively.

$$P_{Gm} - P_{Dm} - V_{0m} \sum_{n=1}^{NB} V_{0n} [B_{mn} \sin(\delta_m - \delta_n) + G_{mn} \cos(\delta_m - \delta_n)] = 0 \quad (19)$$

$$Q_{Gm} - Q_{Dm} - V_{0m} \sum_{n=1}^{NB} V_{0n} [B_{mn} \sin(\delta_m - \delta_n) + G_{mn} \cos(\delta_m - \delta_n)] = 0 \quad (20)$$

In addition, the among the m^{th} bus and n^{th} bus, the TC is denoted as B_{mn} . The magnitude of the output voltage as well as the generator RP need to be maintained within the limits during the designing of a power system. Eq. (21) represents the mathematical formula for the upper limit.

$$V_{Gm}^{\min} \leq V_{Gm} \leq V_{Gm}^{\max}, m = 1, 2, \dots, NG \quad (21)$$

In addition, the lower limit of output voltage of generator is expressed in Eq. (22).

$$Q_{Gm}^{\min} \leq Q_{Gm} \leq Q_{Gm}^{\max}, m = 1, 2, \dots, NG \quad (22)$$

In shunt VAR compensators, the real power outputs limits (lower and upper) are made and it is based on Eq. (23).

$$Q_{Cm}^{\min} \leq Q_{Cm} \leq Q_{Cm}^{\max}, m = 1, 2, \dots, NC \quad (23)$$

In case of the transformer tap settings, the physical considerations exhibit the upper and lower limit values. This is expressed as per Eq. (24).

$$T_m^{\min} \leq T_m \leq T_m^{\max}, m = 1, 2, \dots, NT \quad (24)$$

in PQ buses, the security constrain are based on the voltage magnitude and TLs loadings. The concerned limit flow of each line for the voltage of the buses is shown in Eq. (25) and Eq. (26), respectively.

$$V_{Lm}^{\min} \leq V_{Lm} \leq V_{Lm}^{\max}, m = 1, 2, \dots, NPQ \quad (25)$$

$$H_{im} \leq H_{im}^{\max}, m = 1, 2, \dots, N \quad (26)$$

4. TU-WPA Algorithm for ORPD Problem : Solution Encoding

4.1 Solution Encoding

To solve the problem of ORPD, the TU-WPA optimization Algorithm is introduced. The TU-WPA algorithm takes the input as real power (Q), voltage magnitude (Vo) and transformer tap setting (T).

4.2 TU-WPA model

WOA has taken as one amongst the renowned “nature-inspired meta-heuristic optimization algorithm, which follows the social behavior of the humpback whales”. The standard WOA [31] is good in solving complex and realistic optimization issues. But, it suffers from lower convergence. Typically, PSO [29] is considered as a problem-solving and swarm-based foraging optimization algorithm in which the individuals are defined as particles. On the other hand, the PSO algorithm has higher convergence, yet here the local optimal issues are higher. Thus, the TU-WPA [24] algorithm is introduced here, which is a hybrid algorithm that combines the working principle of PSO and WOA.

The procedure of TU-WPA algorithm is as follows:

Step 1: The search agents of PSO and WOA are initialized as X_e .

Step 2: Then, the fitness is calculated for whole search agents. Here, X_e^* = optimal search agent. The vector position of best solution is denoted as X_e^* .

Step 3: while $tr < \max tr$. Here tr denotes the present generation.

Step 4: Then, for whole search agent, Update a_e , A_e , r_e and p_e . The vector coefficients are determined as A_e and C_e , which is computed as per the Eq. (27) and (28).

$$A_e = 2a_e \cdot r_e - a_e \quad (27)$$

$$C_e = 2 \cdot r_e \quad (28)$$

In the respective equations, a_e value get minimized sequentially from 2 to 0, and random vector r_e is enclosed within the interval $[0, 1]$. Then, $tr = 0$ is set.

Step 5: if ($tr < 20$) and if ($p_e < 0.5$) and if $|A_e| < 1$, then update the agent location by Eq. (30).

$$D_e = |C_e \cdot X_e^*(tr) - X_e(tr)| \quad (29)$$

$$X_e(tr+1) = X_e^*(tr) - A_e - D_e \quad (30)$$

Step 6: if $|A_e| \geq 1$, then pick up an arbitrary search agent X_{earb} and update the agent location by Eq. (31). Here X_{earb} indicates the randomly selected value from the current population.

$$X_e(tr+1) = X_{earb} - D_e \cdot A_e \quad (31)$$

Generally, the whales do random search with respect to the location of other whale. thus, $A_e > 1$ or $A_e < -1$ is used to skip the whales that are far away from them.

Step 7: if $(p_e \geq 0.5)$, then agent location of current search agent is updated by Eq. (33). This expression is the spiral equation is arithmetically defined for the distance among location of prey and humpback whale.

$$D_e' = |X_e^*(tr) - X_e(tr)| \quad (32)$$

$$X_e(tr+1) = D_e' \cdot e^{df} \cdot \cos(2\pi f) + X_e^*(tr) \quad (33)$$

In this, logarithmic spiral shape is defined as d and is termed to be constant, the uniform distribution of random number f falls within the range $[-1, 1]$.

Step 8: if $(tr > 20)$, then update the location on the basis of PSO update in Eq. (7.13) and set $tr = 0$.

Step 9: Check, whether any of the search agent has gone beyond the limit of the search space. Then, calculate fitness for whole search agents. Further, Update X_e^* when other optimal solution subsists. Further, increase $tr = tr + 1$

Step 10: Terminate

5. Results and Discussions

5.1. Simulation Procedure

The proposed ORPD model with the aid of the optimization algorithm was implemented in MATLAB, and the outcomes are observed on “IEEE 14 and the IEEE 39 standard bus systems”. Moreover, the performance of the TU-WPA model was distinguished with four well-known optimization models namely, GA [27], FF [28], PSO [29], ABC [30], WOA [31], DA [32] and CS [33]. This evaluation is made in term of statistical evaluation. “As the entire schemes were stochastic in nature a, respectively and they were greatly based on the initial arbitrary solutions, the arithmetical examination was made by carrying out tests for almost five times”.

5.2. Statistical Evaluation on IEEE 14 Bus System

The TU-WPA approach is compared over the extant models and the resultant acquired are shown graphically in Fig.1. From the resultants it is much clear that the TU-WPA has attaining better ORPD, while compared over the existing ones. On observing the best performance of the adopted scheme, a higher value (0.35327) is recorded, while compared over to the other models GA= 0.26496, FF= 0.27496, PSO= 0.256, ABC= 0.3296, WOA= 0.20333, DA= 0.29432 and CS= 0.30496. Then, on the other hand, the mean performance of the TU-WPA is 0.35462, which is 17.7%, 14.2%, 29.4%, 25.2% and 11% much superior to the existing models like “GA, FF, PSO, ABC, WOA, DA and CS”, respectively. Thus from the overall evaluation, it is clear that the TU-WPA is much superior to the existing works, while implemented under IEEE 14 bus system.

Fig. 1. Statistical analysis on TU-WPA over existing works for IEEE 14 bus system

5.3 Statistical Evaluation on IEEE 39 Bus System

The statistical analysis of the adopted scheme for “IEEE 39 bus system” can be obtained as shown in Fig.2. The highest best value is 38.192 and it is 48.5%, 45.3%, 40%, 25% and 20.6% more superior to the extant models like “GA, FF, PSO, ABC, WOA, DA and CS”, respectively. The median of the TU-WPA model is 36.286, which is the highest among all other models. Thus, from the overall evaluation, it is vivid that TU-WPA model is good in solving ORPD issues.

Fig. 2. Statistical analysis on TU-WPA over existing works for IEEE 39 bus system

5.4 Convergence Analysis

Fig.3 exhibits the convergence analysis of the TU-WPA model by varying the parameter α (fitness function). This variation in fitness is made from “ $\alpha=1$, $\alpha=1.5$, $\alpha=2$, $\alpha=2.5$, $\alpha=3$, $\alpha=3.5$ and $\alpha=4$ ”. Then for each of the variation, the change in the “loss, voltage penalty and final cost function” is computed for both the bus system. The loss function (LSI) of IEEE 14 bus is constant and it is verified from the resultant shown in Fig. 3 (a). for all variation the fitness, the loss function stays at the level of 0.9. Then, in case of voltage penalty (VSI), the TU-WPA has recorded the lowest value as 0.72 at $\alpha=2$. The final cost function is lower for the TU-WPA at $\alpha=1$. On the other hand, the values of “loss, voltage penalty” and final cost function are measured for IEEE 39 bus systems are shown in Fig. 3 (b). The minimal loss function is recorded by the TU-WPA as 0.81 at $\alpha=4$. The final cost value is 1.8, 1.5, 1.29, 1.27, 1.27, 1.54 and 1.81 at $\alpha=1$, $\alpha=1.5$, $\alpha=2$, $\alpha=2.5$, $\alpha=3$, $\alpha=3.5$ and $\alpha=4$, respectively.

Fig. 3. Performance analysis of TU-WPA over existing models for (a) IEEE 14 bus systems and (b) IEEE 39 bus system

6. Conclusion

In this paper a new approach was developed for solving the issues related to the ORPD. The inequality and equality constraints were considered for solving the non-linear optimization problem and the AP loss and the VD minimization was the major objective of this research. Here, a hybrid algorithm referred as TU-WPA was used for optimization issue. The TU-WPA model's performance was verified over other existing algorithms for both the "IEEE 14 and the IEEE 39 benchmark bus systems". On observing the best performance of the adopted scheme in case IEEE 14 bus system, a higher value (0.35327) was recorded, when compared to the other models GA= 0.26496, FF= 0.27496, PSO= 0.256, ABC= 0.3296, WOA= 0.20333, DA= 0.29432 and CS= 0.30496. Thus, the betterment of the adopted work has been validated in an effective manner.

Compliance with Ethical Standards

Conflicts of interest: Authors declared that they have no conflict of interest.

Human participants: The conducted research follows the ethical standards and the authors ensured that they have not conducted any studies with human participants or animals.

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