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Journal of Computational Mechanics, Power System and Control

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Received 21 May, Revised 22 June, Accepted 8 July

Optimal Allocation of UPQC for Power Quality Enhancement via GWO-SA Algorithm

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Abstract: "Unified Power Quality Conditioner (UPQC)" is deployed in power systems for overcoming the issues related with voltage dips or rises in source voltage. Moreover, it controls the load voltage and mitigates the entire problems related with voltage and current harmonics, thereby enhancing the power quality (PQ). Here, this work presents a PQ enhancement approach by integrating the optimization concept. For optimization purpose, this work deploys the "Grey Wolf Optimization with Self-adaptiveness (GWO-SA)" model. Here, the presented model determines the optimal allocation of UPQC by taking into consideration of power system loss, UPQC cost and stability as well. Further, the superiority of GWO-SA is validated and compared over existing works with respect to varied measures such as cost and location analysis. From the analysis, the performance of the implemented work when the number of location=1 is 0.21%, 0.59%, 0.77% and 0.26% better than SLnO, GWO, DA and PSO, respectively at 0% loading condition.

Keywords: UPQC; D-FACTS device; DSTATCOM; Voltage stability; GWO-SA model.

Nomenclature

Abbreviations	Descriptions
APF	Active Power Filters
BFSLF	Backward/Forward Sweep Load Flow
CS	Cuckoo Search
DSTATCOM	Distribution Static Compensator
DA	Dragonfly Optimization
EE	Energy Efficiency
FF	Firefly
GWO-SA	Grey Wolf Optimization With Self-Adaptiveness
MOPSO	Multi-Objective Particle Swarm Optimisation
PV	Photovoltaic
PF	Power Factor
PQ	Power Quality
PCC	Point Of Common Coupling
PSO	Particle Swarm Optimization
RDN	Radial Distribution Networks
SEU	Series Unit
SLnO	Sea Lion Optimization
SSVR	Static Series Voltage Regulator
THD	Total Harmonic Distortion
UPQC	Unified Power Quality Conditioner
UPQC-O	Open UPQC
VSI	Voltage Stability Index

1. Introduction

The most important objective of power system operations is efficiency. Power losses and voltage limits acts a key role in proficient functioning of electrical system. Therefore, sustaining the voltage within the allowable limits is significant for the better performance of the system [6]. There are diverse devices to

manage the issues on voltage enhancement namely, series capacitors, voltage regulators and so on. However, the disadvantages with these devices are resonance and slower response [7].

SSVR is a D-FACTS device utilized for enhancing the voltages in distribution network. The shunt D-FACT device termed as DSTATCOM offers reactive power compensation for reducing power loss. Diverse optimization techniques like PSO, FF and so on were exploited for optimal allocation of D-STATCOM [8]. The functionalities of shunt and series D-FACTS are offered by UPQC. UPQC is a versatile D-FACTS device used for enhancing the voltage and for minimizing the power loss in network [9].

The UPQC comprises of 2 voltage source inverters, which were linked to a DC energy storing capacitor, which could be deployed to improve flickers, unbalances, and harmonics, as well as voltage sags, dynamic reactive and active power regulations [10] [11]. The series component introduces voltage for balancing the network with zero distortion. Likewise, UPQC shunt component feeds balances the current at PCC bus in a sinusoidal manner [12] [13]. To carry out this operation, shunt capacitors are deployed. Moreover, optimal allocation and rating of these capacitors is necessary as it assists in reducing the power losses in the network

The arrangement of the work is specified as: Section II portrays the review. Section III explains the UPQC model and section IV portrays the optimal allocation and sizing of UPQC via GWO-SA algorithm. Section V illustrates the outcomes and the paper is summarized in section VI.

2. Literature Review

2.1 Related works

In 2018, Ganguly and Lakshmi [1] have presented a novel allocation approach for UPQC-O incorporated PV generation system in RDN for improving the PQ and EE. In addition, the operational parameters like bus voltage were determined via "forward-backward sweep load flow". Moreover, PSO was exploited that determined the optimal allocation of UPQC in RDN networks.

In 2020, Jian et al. [2] have presented an optimal approach for UPQC that depends on hierarchical metaheuristic concept. In addition, the adopted model takes account of 3 objectives that included (a) minimization of load voltage variation and (b) maximization of PF; (c) minimization of the total UPQC power. These objectives were partitioned in to varied multi objectives for attaining better solution. Eventually, analysis was carried out that proved the supremacy of the adopted scheme.

In 2019, Lakshmi and Sanjib [3] have presented a multi-objective framework for optimally allocating open UPQC for saving the peak load of RDNs. The adopted model aided in mitigating various PQ issues. Here, maximal attainment of peak load saving, minimizing placement cost of UPQC-O, and minimizing total power loss were considered as the objectives. Moreover, MOPSO was deployed for optimizing these objectives that offered better solutions.

In 2016, Kumara and Srikanth [4] have developed FF and CS models for optimal allocation of UPFC, which in turn improved the stability of the system. Here, the FF approach has optimized the maximal power loss via appropriate position of UPFC. Moreover, the dynamic stability parameters were restored into secured limits by means of optimal UPFC capacity that in turn resulted in minimized cost.

In 2020, Ali and Amini [5] have presented a precise modelling of UPQC-O along with its incorporation in BFSLF. Moreover, the performance of SEU that was accountable for voltage sag compensation was limited in this work. In addition, an operational technique was introduced for improving the SEU performance. Finally, evaluation was carried out the portrayed the development of the presented model in overcoming minimal voltage sags.

3. UPQC Model

The model of UPQC is revealed in Fig 1. The UPQC involves series APF as well as shunt APF. Here, the latter one is connected across the loads that resolve the issues namely, "power factor enhancement, reactive power compensation, compensation of load unbalance, current harmonic and dc link voltage control". Accordingly, the series APF performs as controlled voltage source that resolves issues such as flicker, voltage harmonics and so on. The UPQC lessens the load interruption zone into a normal operating zone. Also, it reduces the voltage sags and unbalances, which in turn minimizes the power loss. The operation of shunt inverter and series inverter is depicted as follows: the series inverter voltage, $V_{\rm se}$ depends on maximal voltage sag that must be reduced. The source voltage magnitudes during voltage sags and usual states are signified as $V_{\rm s}=V_{\rm SO}$ and $V_{\rm s}=mV_{\rm SO}$. Here, $m_{\rm sag}=\left(1-m\right)$. At all conditions, load

voltage, $V_L = V_{SO} = V_s$. The requisite series voltage inoculation for minimizing m_{sag} p.u of sags is computed as shown in Eq. (1).

$$\begin{split} V_{\rm se} &= \sqrt{V_{\rm L}^2 + (mV_{\rm SO})^2 - 2V_{\rm L}(mV_{\rm SO})\cos\delta} \\ &= V_{\rm s}\sqrt{1 + m^2 - 2m\cos\delta} \end{split} \tag{1}$$

Accordingly, $mV_sI_s = V_LI_L\cos\phi$ delivers source current as per Eq. (2), here I_L and I_s refers to loading current and compensated source-end current in that order. In Eq. (1) and (2), VA ratings of series inverter are computed as per Eq. (3).

$$I_{s} = I_{L} \cos \phi / m \tag{2}$$

$$S_{se} = V_{se}I_{s} = V_{s}I_{L}\cos\phi\sqrt{1 + m^{2} - 2m\cos\delta/m}$$
(3)

Eq. (5) and (4) reveals the reactive and active powers generated by series inverter, here, $\theta_{\rm se} = 180^{\circ} - \tan^{-1}(\sin \delta/1 - \cos \delta)$ [14].

$$P_{\rm se} = S_{\rm se} \cos \theta_{\rm se} \tag{4}$$

$$M_{se} = S_{se} \sin \theta_{se} \tag{5}$$

Eq. (6) shows the formulation of current via shunt inverter $I_{\rm sh}$.

$$I_{sh} = \sqrt{I_s^2 + I_L^2 - 2I_sI_L\cos(\phi - \delta)}$$

$$= I_L\sqrt{1 + \cos^2\phi/m^2 - 2\cos\phi\cos(\phi - \delta)/m}$$
(6)

Furthermore, the shunt inverter carries out compensation of harmonics in load end as specified in Eq. (7) and (8), where I_{sh}^{di} and I_{L}^{di} points out distortion element of shunt and load, I_{sh}^{fu} and I_{L}^{fu} points out fundamental component of shunt and load, I_{L}^{fu} and I_{L}^{fu} points out fundamental component of shunt and load, I_{L}^{fu} and I_{L}^{fu} and I_{L}^{fu} points out fundamental component of shunt and load, I_{L}^{fu} and I_{L}^{fu} and I_{L}^{fu} and I_{L}^{fu} points out fundamental component of shunt and load, I_{L}^{fu} and I_{L}^{fu} and I_{L}^{fu} points out fundamental component of shunt and load, I_{L}^{fu} and I_{L}^{fu} points out fundamental component of shunt and load, I_{L}^{fu} and I_{L}^{fu} points out fundamental component of shunt and load, I_{L}^{fu} and I_{L}^{fu} points out fundamental component of shunt and load, I_{L}^{fu} and I_{L}^{fu} points out fundamental component of shunt and load, I_{L}^{fu} and I_{L}^{fu} points out fundamental component of shunt and load, I_{L}^{fu} and I_{L}^{fu} points out fundamental component of shunt and load, I_{L}^{fu} and I_{L}^{fu} points out fundamental component of shunt and load, I_{L}^{fu} and I_{L}^{fu} points out fundamental component of shunt and load, I_{L}^{fu} and I_{L}^{fu} points out fundamental component of shunt and load, I_{L}^{fu} and I_{L}^{fu} points out fundamental component of shunt and load of the shunt and l

$$I_{L}^{di} = I_{sh}^{di} \tag{7}$$

$$T_{L}I_{L}^{fu} = T_{sh}I_{sh}^{fu} \tag{8}$$

Thus, r.m.s of shunt current is determined as in Eq. (9) and its VA rating is specified as in Eq. (10).

$$I_{\rm sh} = I_{\rm sh}^{\rm fu} \sqrt{1 + T_{\rm sh}^2}$$

$$= I_{\rm I}^{\rm fu} \sqrt{1 + \cos^2 \phi / m^2 - 2\cos \phi \cos(\phi - \delta) / m + T_{\rm L}^2}$$
(9)

$$\begin{split} S_{sh} &= V_s I_{sh} \\ &= V_s I_L^{fu} \sqrt{1 + \cos^2 \phi / m^2 - 2 \cos \phi \cos (\phi - \delta) / m + T_L^2} \end{split} \tag{10}$$

Eq. (11), (12) and Eq. (13) illustrates the active, reactive powers and total reactive power delivered by shunt inverter. $\theta_{sh} = tan^{-1} \{cos(\phi - \delta) - cos\phi/sin(\phi - \delta)\} + 90^{\circ} - \delta$.

$$P_{\rm sh} = S_{\rm sh} \cos \theta_{\rm sh} \tag{11}$$

$$M_{\rm sh} = S_{\rm sh} \sin \theta_{\rm sh} \tag{12}$$

$$M_{UPQC} = M_{se} + M_{sh} \tag{13}$$

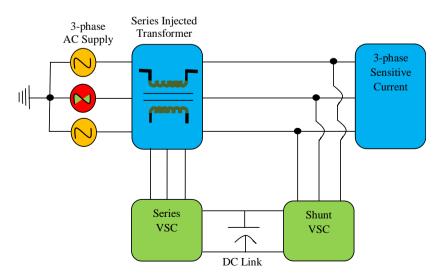


Fig. 1. Pictorial representation of UPQC

3.1 Objective Model

In fact, the placement of UPQC should satisfy the objectives for enhancing PQ. Eq. (14) demonstrates the objectives of presented scheme. Eq. (17) shows Lo computation, where O_k points out conductance of m^{th} line and voltage angles of i and j buses is signified as δ_i and δ_i . The cost of UPQC is specified by Eq. (15), where, nUPQC points out UPQC's longevity, O points out UPQC's operating level in MVAr, UPQC Cost, points out annual cost of UPQC, UPQC points out investment cost, R points out asset rate of return. The VSI is measures as in Eq. (16), where μ points out a constant, V^b points out voltage magnitude for bth bus.

$$OB = \min(UPQC_{cost} + Lo + VSI)$$
(14)

$$UPQC_{Cost}(US(\$/kVAr)) = 0.0003O^2 - 0.2691O + 188.22$$

$$\begin{split} &UPQC_{Cost_{year}} = UPQC_{Cost} \frac{\left(l-R\right)^{nUPQC} \times R}{\left(l+R\right)^{nUPQC} - 1} \\ &VSI = \begin{cases} 1 & \text{if} \quad V^{min} \leq V^b \leq V^{max} \\ \exp\left(\mu \mid l - V^b \mid\right) & \text{otherwise} \end{cases} \end{split} \tag{15}$$

$$VSI = \begin{cases} 1 & \text{if} \quad V^{\min} \le V^{b} \le V^{\max} \\ \exp(\mu \mid 1 - V^{b} \mid) & \text{otherwise} \end{cases}$$
 (16)

$$Lo = \sum_{m=1}^{N_L} Lo_m = \sum_{m=1}^{N_L} O_m \left\{ V_i^2 + V_j^2 - 2V_i V_j \cos(\delta_i - \delta_j) \right\}$$
 (17)

The inequality and equality constraints are briefed below.

Equality Constraints

In fact, the line powers are addressed by voltage magnitude and phase angles [15]. Eq. (18) and Eq. (19) shows the active and reactive power balances respectively.

$$P_{H_{i}} - P_{E_{i}} - \sum_{m=1}^{N_{L}} o_{im} \left\{ V_{i}^{2} + V_{j}^{2} - 2V_{i}V_{j}\cos(\delta_{i} - \delta_{j}) \right\} = 0$$
(18)

$$\mathbf{M}_{H_{i}} - \mathbf{M}_{E_{i}} - \sum_{m=1}^{N_{L}} \mathbf{p}_{im} \left\{ V_{i}^{2} + V_{j}^{2} - 2V_{i}V_{j} \sin(\delta_{i} - \delta_{j}) \right\} = 0$$
 (19)

In Eq. (18) and (19), $P_{\rm H_i}$ and $P_{\rm E_i}$ points out active power and active power demand at ith bus, $P_{\rm loss}$ points out total active power loss. M_{H_i} and M_{E_i} points out reactive power and m reactive power demand at i^{th} bus, Q_{loss} indicates the reactive power loss. o_{i-j} and p_{i-j} points out conductance and susceptance among i and j. V_i and V_i points out voltage magnitude of i and j buses.

Inequality Constraints

These constraints are classified into major groups.

Line flow limit: The constraint for power flow limit is determined as per Eq. (20), here S_max points out highest power flow value at mth line.

$$SE_{m} \leq SE_{mmax}$$
 (20)

Bus voltage limit: It takes account of both voltage unbalance and magnitude limit nodes based on the condition specified in Eq. (21).

$$V^{\min} < V < V^{\max} \tag{21}$$

4. Optimal Allocation And Sizing of UPQC Via GWO-SA Algorithm

4.1 Solution Encoding

For attaining the objectives, the size and positions of UPQC on "IEEE 33 bus system and the IEEE 69 bus systems" are given as solutions as shown in Fig. 2, where Pt a points out the bus line positions and Si_{z_N} points out UPQC size. Here, a =1,2,3..N, in which, N = 33 and N = 69 for IEEE 33 and IEEE 69 bus systems, correspondingly.

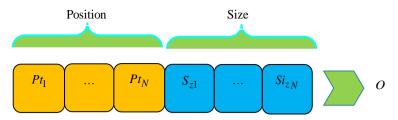


Fig. 2. Solution encoding

4.2 GWO-SA Algorithm

The GWO [13] portrays the hunting characteristics of grey wolves and its control hierarchy. Four kinds of wolves namely, α , η , ζ , ω are considered for performing the headship hierarchy. The wolves namely, α , η and ζ are involved in hunting process. Among them α takes decision on hunting model and sleeping locations, η and ζ aids α in taking choices. The encircling nature of wolves are revealed as in Eq. (22) and Eq. (23), here X and Y represent the coefficient vectors, O_p and O indicate position vector of prey and grey wolves and t indicate the current iteration. Consequently, X and Y is computed as per Eq. (24) and Eq. (25), and r_1 and r_2 reveal the arbitrary vectors amongst [0, 1]. As per GWO-SA model, α is calculated as per Eq. (26), here τ indicates the change of fitness as shown in Eq. (27), if α if α is calculated. In Eq. (27), α f(t-1) and f(t) points out the previous and present iterations in that order.

$$Z = |Y.O_{p}(t) - O(t)|$$
(22)

$$O_{p}(t+1) = O_{p}(t) - X.Z$$
 (23)

$$X = 2a.r_1 - a \tag{24}$$

$$Y = 2r_2 \tag{25}$$

$$a = \tau * \left(2 - 1 * \left(\frac{2}{t_{\text{max}}} \right) \right) \tag{26}$$

$$\tau = \frac{\left(f(t-1) - f(t)\right)}{f(t-1)} \tag{27}$$

The arithmetical formulation for illustrating the hunting character of wolf is exposed by Eq. (28) to Eq. (33) and the final position of wolves is revealed in Eq. (34).

$$Z_{\alpha} = |Y_1 - O_{\alpha} - O| \tag{28}$$

$$Z_{\eta} = \left| Y_2 - O_{\eta} - O \right| \tag{29}$$

$$\mathbf{Z}_{r} = \left| \mathbf{Y}_{3} - \mathbf{O}_{r} - \mathbf{O} \right| \tag{30}$$

$$O_1 = O_\alpha - X_1 \cdot (Z_\alpha) \tag{31}$$

$$O_2 = O_n - X_2 \cdot (Z_n) \tag{32}$$

$$O_3 = O_{\zeta} - X_3 \cdot (Z_{\zeta}) \tag{33}$$

$$O(t+1) = \frac{O_1 + O_2 + O_3}{3}$$
 (34)

5. Results and Discussions

5.1 Simulation Procedure

The presented approach was executed in MATLAB and the outcomes were observed. This work considered 2 diverse bus systems such as "IEEE 69 bus system and IEEE 33 bus system". In addition, 3 experiments were done based on UPQC allocation (i) 1 location (ii) 2 locations (iii) 3 locations. Furthermore, the analysis of presented model was carried out by altering the loading conditions to "0%, 50%, 100%, 150%, 200%, and 250%" correspondingly. Here, the supremacy of presented model was proved over the existing models such as SLnO [16], GWO [21], DA [18] and PSO [19].

5.2 Performance Analysis: IEEE 33 Bus System

This division portrays the analysis of the presented work over the existing works for "IEEE 33 bus system" for varied number of locations such as 1, 2, and 3. The performance of the implemented work when the number of location=1 is shown in Table II. On observing the Table, the GWO-SA model has achieved a higher performance than existing schemes with respect to reduced fitness value. Table II reveals the analysis of presented work over the existing works when the number of location=2. On examining Table I, the GWO-SA model at 0% loading condition is 0.21%, 0.59%, 0.77% and 0.26% better than SLnO, GWO, DA and PSO, respectively. Likewise, for all loading conditions, the presented work has attained optimal outcomes than the existing ones.

Table 1: Performance of presented work over existing works for varied Loading Conditions (location count = 1)

Loading (%)	SLnO	GWO	DA	PSO	GWO-SA
0	515.15	517.12	518.07	515.4	514.08
50	556.84	561.09	561.28	561.19	553.8
100	599.91	599.91	599.91	599.91	592.91
150	642.25	644.29	642.58	642.46	641.22
200	690.79	690.9	694.03	691.02	688.7
250	740.57	742.06	740.85	740.81	739.43

Table 2: Performance of presented work over existing works for varied Loading Conditions (location count = 2)

Loading (%)	SLnO	GWO	DA	PSO	GWO-SA
0	412.36	420.27	420.27	420.85	410.9
50	458.13	456.73	457.22	457.22	459.07
100	495.2	493.03	495.19	495.78	493.69
150	543.16	541.1	541.74	541.3	533.19
200	589.88	587.25	589.33	588.94	585.07
250	638.06	636.73	647.16	638.06	634.96

Table 3: Performance of presented work over existing works for varied Loading Conditions (location count = 3)

Loading (%)	SLnO	GWO	DA	PSO	GWO-SA
0	378.1	379.68	387.59	378.17	377.06
50	422.47	424.16	430.56	422.88	423.02
100	460.17	460.39	472.61	459.91	455.06
150	506.88	508.27	514.98	514.54	510.25
200	555.97	554.82	562.81	554.68	553.32
250	603.71	605.33	612.77	606.04	604.2

5.3 Performance Analysis: IEEE 69 Bus System

The analyses of presented work over existing works for "IEEE 69 bus system" are described in this subdivision. The analysis was made by varying the loading conditions for varied location counts (1, 2 and 3). Table IV demonstrates the analysis when number of location is one, Table V shows the outcomes when location count is 2 and Table VI demonstrates the analysis when number of location is three. On examining the outcomes, the presented model has satisfied the objective function in an optimal way when evaluated over the existing works.

Table 4: Performance of presented work over existing works for varied Loading Conditions (location count = 1)

Loading (%)	SLnO	GWO	DA	PSO	GWO-SA
0	543.21	543.21	537.99	543.21	536.64
50	555.86	555.86	555.86	549.37	549.35
100	569.88	563.42	569.88	570.68	563.42
150	585.31	580.07	585.31	580.07	580.07
200	605.71	604.95	605.35	604.95	598.63
250	623.4	623.4	618.15	623.4	617.11

Table 5: Performance of presented work over existing works for varied Loading Conditions (location count = 21)

Loading (%)	SLnO	GWO	DA	PSO	GWO-SA	
0	446.07	433.2	443.55	433.39	432.14	
50	446.01	445.8	457.37	455.8	453.1	
100	460.99	473.05	473.05	467.66	459.75	
150	484.71	475.12	488.34	474.89	474.46	
200	491.65	491.94	491.87	493.81	491.78	
250	513.18	513.03	521.19	524.05	513.81	

Table 6: Performance of presented work over existing works for varied Loading Conditions (location count = 3)

Loading (%)	SLnO	GWO	DA	PSO	GWO-SA
0	402.25	400.03	400.33	400.42	395.65
50	412.89	412.69	414.42	412.94	412.79
100	429.27	426.93	426.79	424.22	426.71
150	444.67	442.32	442.39	441.61	441.19
200	458.7	458.73	460.98	458.64	459.13
250	482.47	480.06	480.81	477.75	476.13

6. Conclusion

This work has presented a new PQ enhancement model depending on a GWO-SA approach. For enhancing the PQ, it was essential for determining the optimal position and sizing of UPQC. Here, GWO-SA was exploited with the objective of minimizing cost, power loss, and stability as well. Finally, evaluation was carried out to establish the enhancement of the adopted model. On examining the outcomes, the implemented work at 0% loading condition was 0.21%, 0.59%, 0.77% and 0.26% better than SLnO, GWO, DA and PSO, respectively. Likewise, for all loading conditions, the presented work has attained optimal outcomes than the existing ones.

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